

# Chapter 9

## DESIGN OF NONRECURSIVE (FIR) FILTERS

### 9.1 Introduction

#### 9.2.1 Properties of Constant-Delay Nonrecursive Filters

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Victoria, BC, Canada  
Email: [aantoniou@ieee.org](mailto:aantoniou@ieee.org)

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- In certain filtering applications, delay distortion is highly undesirable and in such applications digital filters are required that have a *linear-phase response*.
- It turns out that linear-phase response can be easily achieved by designing the required filter as a nonrecursive filter.
- A linear-phase response is obtained by simply ensuring that the impulse response satisfies certain symmetry conditions.
- In this presentation, some basic properties of linear-phase nonrecursive filters are examined.

## Constant Delay in Nonrecursive Filters

- A causal nonrecursive filter can be represented by the transfer function

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- Its frequency response is given by

$$H(e^{j\omega T}) = M(\omega)e^{j\theta(\omega)} = \sum_{n=0}^{N-1} h(nT)e^{-j\omega nT}$$

where

$$M(\omega) = |H(e^{j\omega T})| \quad \text{and} \quad \theta(\omega) = \arg H(e^{j\omega T})$$

...

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- The absolute delay, which is also known as the *phase delay*, and the *group delay* of a filter are given by

$$\tau_p = -\frac{\theta(\omega)}{\omega} \quad \text{and} \quad \tau_g = -\frac{d\theta(\omega)}{d\omega}$$

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$$\tau_p = -\frac{\theta(\omega)}{\omega} \quad \text{and} \quad \tau_g = -\frac{d\theta(\omega)}{d\omega}$$

- If both the phase and group delays are assumed to be constant, then the phase response must be linear, i.e.,

$$\theta(\omega) = -\tau\omega = \tan^{-1} \frac{-\sum_{n=0}^{N-1} h(nT) \sin \omega nT}{\sum_{n=0}^{N-1} h(nT) \cos \omega nT}$$

where  $\tau$  is a constant.

## Constant Delay in Nonrecursive Filters *Cont'd*

...

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- Hence

$$\tan \tau\omega = \frac{\sum_{n=0}^{N-1} h(nT) \sin \omega nT}{\sum_{n=0}^{N-1} h(nT) \cos \omega nT}$$

or

$$\sum_{n=0}^{N-1} h(nT) (\cos \omega nT \sin \omega\tau - \sin \omega nT \cos \omega\tau) = 0$$

and so

$$\sum_{n=0}^{N-1} h(nT) \sin(\omega\tau - \omega nT) = 0$$

...

$$\sum_{n=0}^{N-1} h(nT) \sin(\omega\tau - \omega nT) = 0$$

- The solution of the above equation can be shown to be

$$\tau = \frac{1}{2}(N-1)T$$

$$h(nT) = h[(N-1-n)T] \quad \text{for } 0 \leq n \leq N-1$$

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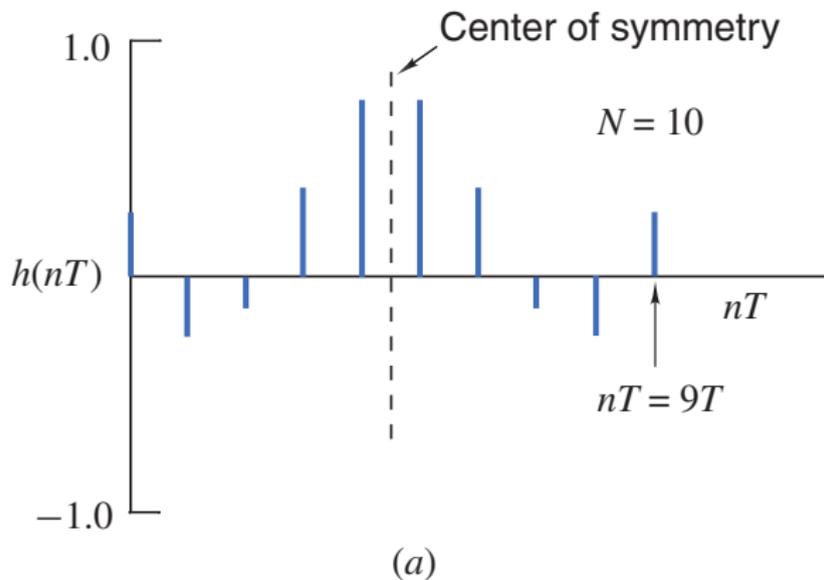
$$\tau = \frac{1}{2}(N - 1)T$$

$$h(nT) = h[(N - 1 - n)T] \quad \text{for } 0 \leq n \leq N - 1$$

- Therefore, a nonrecursive filter can be designed to have *constant phase and group delays* over its entire baseband by simply ensuring that its impulse response is *symmetrical* about its center.

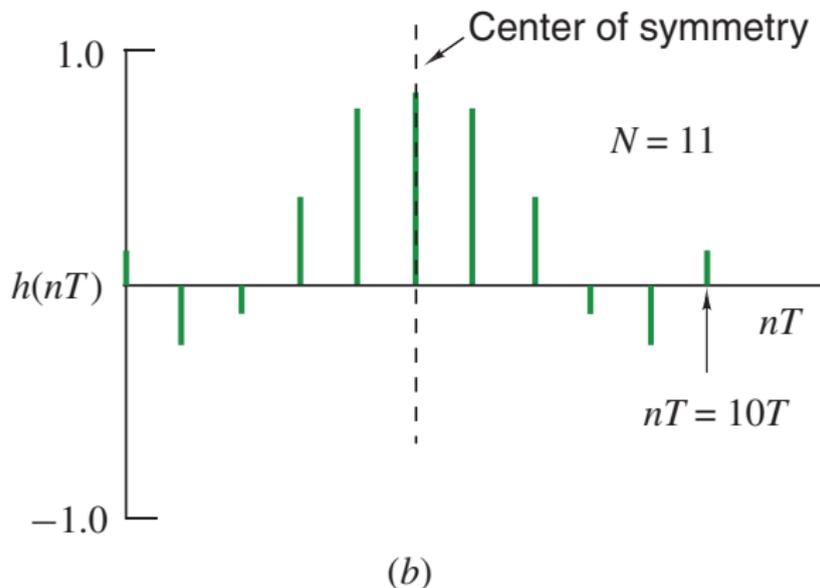
## Constant Delay in Nonrecursive Filters *Cont'd*

- For *even*  $N$ , the impulse response is symmetrical about the midpoint between samples  $(N - 2)/2$  and  $N/2$  as shown:



## Constant Delay in Nonrecursive Filters *Cont'd*

- For *odd*  $N$ , the impulse response is symmetrical about sample  $(N - 1)/2$  as shown:



## Constant Delay in Nonrecursive Filters *Cont'd*

- In most applications only the group delay needs to be constant in which case the phase response can have the form

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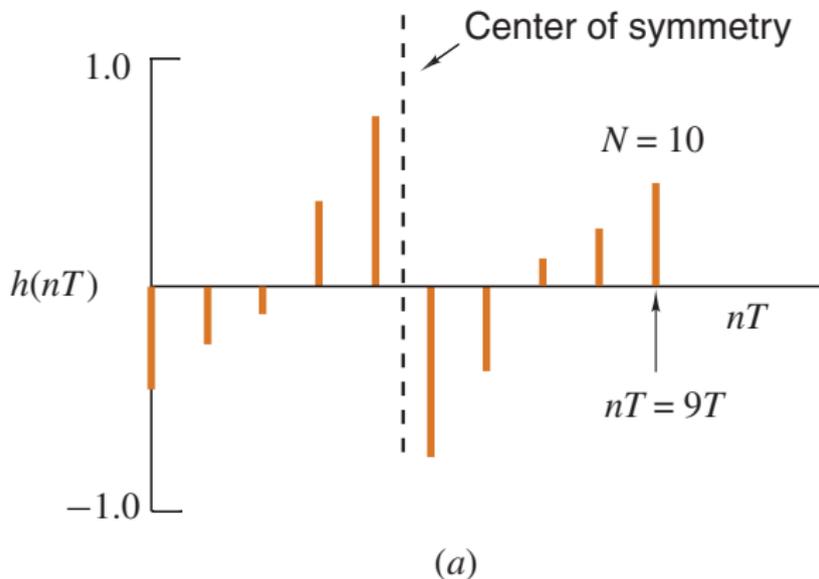
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$$\begin{aligned}\tau &= \frac{1}{2}(N-1)T \\ h(nT) &= -h[(N-1-n)T]\end{aligned}$$

- In effect, a nonrecursive filter can be designed to have *constant group delay* over its entire baseband by simply ensuring that its impulse response is *antisymmetrical* about its center.

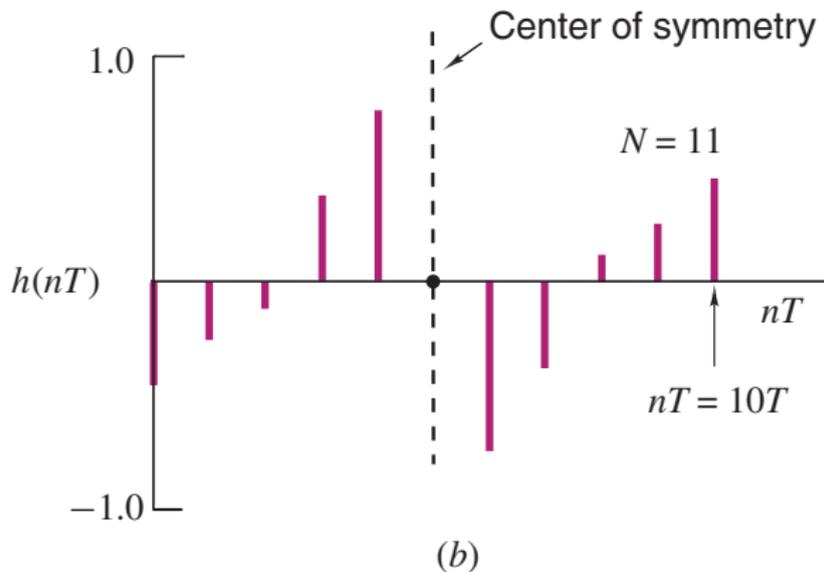
## Constant Delay in Nonrecursive Filters *Cont'd*

- For *even*  $N$ , the impulse response is antisymmetrical about the midpoint between samples  $(N - 2)/2$  and  $N/2$  as shown:



## Constant Delay in Nonrecursive Filters *Cont'd*

- For *odd*  $N$ , the impulse response is antisymmetrical about sample  $(N - 1)/2$  as shown:



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- For the case of a *symmetrical* impulse response and odd  $N$ ,

$$H(e^{j\omega T}) = \sum_{n=0}^{(N-3)/2} h(nT)e^{-j\omega nT} + h\left[\frac{(N-1)T}{2}\right]e^{-j\omega(N-1)T/2} + \sum_{n=(N+1)/2}^{N-1} h(nT)e^{-j\omega nT} \quad (\text{A})$$

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- If we first let  $N - 1 - n = m$  and then let  $m = n$ , we get

$$\begin{aligned} \sum_{n=(N+1)/2}^{N-1} h(nT)e^{-j\omega nT} &= \sum_{n=(N+1)/2}^{N-1} h[(N-1-n)T]e^{-j\omega nT} \\ &= \sum_{n=0}^{(N-3)/2} h(nT)e^{-j\omega(N-1-n)T} \end{aligned} \quad (\text{B})$$

- From Eqs. (A) and (B)

$$H(e^{j\omega T}) = e^{-j\omega(N-1)T/2} \left\{ h \left[ \frac{(N-1)T}{2} \right] + \sum_{n=0}^{(N-3)/2} 2h(nT) \cos \left[ \omega \left( \frac{N-1}{2} - n \right) T \right] \right\}$$

and with  $(N-1)/2 - n = k$ , we have

$$H(e^{j\omega T}) = e^{-j\omega(N-1)T/2} \sum_{k=0}^{(N-1)/2} a_k \cos \omega k T$$

where  $a_0 = h \left[ \frac{(N-1)T}{2} \right]$  and  $a_k = 2h \left[ \left( \frac{N-1}{2} - k \right) T \right]$

# Frequency Response of Nonrecursive Filters *Cont'd*

$h(nT)$	$N$	$H(e^{j\omega T})$
Symmetrical	Odd	$e^{-j\omega(N-1)T/2} \sum_{k=0}^{(N-1)/2} a_k \cos \omega k T$
	Even	$e^{-j\omega(N-1)T/2} \sum_{k=1}^{N/2} b_k \cos[\omega(k - \frac{1}{2}) T]$
Antisymmetrical	Odd	$e^{-j[\omega(N-1)T/2 - \pi/2]} \sum_{k=1}^{(N-1)/2} a_k \sin \omega k T$
	Even	$e^{-j[\omega(N-1)T/2 - \pi/2]} \sum_{k=1}^{N/2} b_k \sin[\omega(k - \frac{1}{2}) T]$

where  $a_0 = h \left[ \frac{(N-1)T}{2} \right]$ ,  $a_k = 2h \left[ \left( \frac{N-1}{2} - k \right) T \right]$ ,  $b_k = 2h \left[ \left( \frac{N}{2} - k \right) T \right]$

## Location of Zeros

- The impulse response symmetry conditions described impose certain restrictions on the zeros of transfer function  $H(z)$ .

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- For *odd*  $N$ , we can write

$$H(z) = \frac{1}{z^{(N-1)/2}} \left\{ \sum_{n=0}^{(N-3)/2} h(nT) (z^{(N-1)/2-n} \pm z^{-[(N-1)/2-n]}) + \frac{1}{2} h \left[ \frac{(N-1)T}{2} \right] (z^0 \pm z^0) \right\} \quad (C)$$

where the negative sign applies to the case of antisymmetrical impulse response.

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- With  $(N-1)/2 - n = k$ , Eq. (C) can be expressed as

$$H(z) = \frac{N(z)}{D(z)} = \frac{1}{z^{(N-1)/2}} \sum_{k=0}^{(N-1)/2} \frac{a_k}{2} (z^k \pm z^{-k})$$

where  $a_0$  and  $a_k$  are given in the table of frequency responses shown earlier.

...

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- If we replace  $z$  by  $z^{-1}$  in  $N(z)$ , we get

$$\begin{aligned} N(z^{-1}) &= \sum_{k=0}^{(N-1)/2} a_k (z^{-k} \pm z^k) \\ &= \pm \sum_{k=0}^{(N-1)/2} a_k (z^k \pm z^{-k}) = \pm N(z) \end{aligned}$$

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- Therefore, if  $z_i = r_i e^{j\psi_i}$  is a zero of  $H(z)$ , then its *reciprocal*  $z_i^{-1} = e^{-j\psi_i} / r_i$  must also be a zero of  $H(z)$ .

## Location of Zeros *Cont'd*

The property  $N(z^{-1}) = \pm N(z)$  imposes the following constraints on the zeros of the transfer function:

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2. An arbitrary number of complex-conjugate pairs of zeros can be located on the unit circle since

$$(z - z_i)(z - z_i^*) = (z - e^{j\psi_i})(z - e^{-j\psi_i}) = \left(z - \frac{1}{z_i^*}\right) \left(z - \frac{1}{z_i}\right)$$

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3. Real zeros off the unit circle must occur in reciprocal pairs.

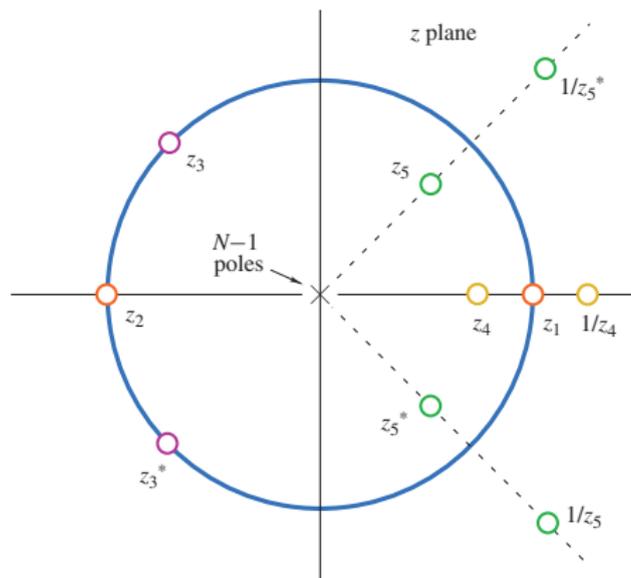
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3. Real zeros off the unit circle must occur in reciprocal pairs.
4. Complex zeros off the unit circle must occur in groups of four, namely,  $z_i$ ,  $z_i^*$ , and their reciprocals.

## Location of Zeros *Cont'd*



*Note:* Polynomials with these properties are called *mirror-image polynomials*.

*This slide concludes the presentation.  
Thank you for your attention.*